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Permanent Link to Space-Time Equalization Techniques for New GNSS Signals
2021/06/12
By Pratibha B. Anantharamu, Daniele Borio, and Gérard Lachapelle Spatial and temporal information of signals received from multiple antennas can be applied to mitigate the impact of new GPS and Galileo signals' binary-offset sub-carrier, reducing multipath and interference effects. New modernized GNSS such as GPS, Galileo, GLONASS, and Compass broadcast signals with enhanced correlation properties as compared to the first generation GPS signals. These new signals are characterized by different modulations that provide improved time resolution, resulting in more precise range measurements, along with the advantage of being more resilient to multipath and RF interference. One of these modulations is the binary-offset-carrier (BOC) modulation transmitted by Galileo and modernized GPS. Despite the benefits of BOC modulation schemes, difficulties in tracking BOC signals can arise. The autocorrelation function (ACF) of BOC signals is multi-peaked, potentially leading to false peak-lock and ambiguous tracking. Intense research activities have produced different BOC tracking schemes that address the issue of multi-peaked BOC signal tracking. Additionally, new tracking schemes including space-time processing can be adopted to further improve the performance of existing algorithms. Space-time equalization is a technique that utilizes spatial and temporal information of signals received from multiple antennas to compensate for the effects of multipath fading and co-channel interference. In the context of BOC signals, these kinds of techniques can be applied to mitigate the impact of the sub-carrier, which is responsible for a multi-peaked ACF, reducing multipath and interference effects. In temporal processing, traditional equalizers in time-domain are useful to compensate for signal distortions. But equalization becomes more challenging in the case of BOC signals, where the effect of both sub-carrier and multipath must be accounted for. On the other hand, by using spatial processing, it should be possible to extract the desired signal component from a set of received signals by electronically varying the antenna array directivity (beamforming). The combination of an antenna array and a

temporal equalizer results in better system performance. Hence the main objective of this research is to apply space-time processing techniques to BOC modulated signals received by an antenna array. The main intent is to enhance the signal quality, avoid ambiguous tracking and improve tracking performance under weak signal environments or in the presence of harsh multipath components. The focus of previous antenna-array processing using GNSS signals was on enhancing GNSS signal quality and mitigating interference and/or multipath related issues. Unambiguous tracking was not considered. Here, we develop a space-time algorithm to mitigate ambiguous tracking of BOC signals along with improved signal quality. The main objective is to obtain an equalization technique that can operate on BOC signals to provide unambiguous BPSK-like correlation function capable of altering the antenna array beam pattern to improve the signal to interference plus noise ratio. Space-time adaptive processing structure proposed for BOC signal tracking; the temporal filter provides signal with unambiguous ACF whereas the spatial filter provides enhanced performance with respect to multipath, interference, and noise. Initially, temporal equalization based on the minimum mean square error (MMSE) technique is considered to obtain unambiguous ACF on individual antenna outputs. Spatial processing is then applied on the correlator outputs based on a modified minimum variance distortionless response (MVDR) approach. As part of spatial processing, online calibration of the real antenna array is performed which also provides signal and noise information for the computation of the beamforming weights. Finally, the signal resulting from temporal and spatial equalization is fed to a common code and carrier tracking loop for further processing. The effectiveness of the proposed technique is demonstrated by simulating different antenna array structures for BOC signals. Intermediate-frequency (IF) simulations have been performed and linear/planar array structures along with different signal to interference plus noise ratios have been considered. A modified version of The University of Calgary software receiver, GSNRx, has been used to simultaneously process multi-antenna data. Further tests have been performed using real data collected from Galileo test satellites, GIOVE-A and GIOVE-B, using an array structure comprising of two to four antennas. A 4-channel front-end designed in the PLAN group, and a National Instruments (NI) signal vector analyzer equipped with three PXI-5661 front-ends (NI 2006) have been used to collect data synchronously from several antennas. The data collected from the antennas were progressively attenuated for the analysis of the proposed algorithm in weak signal environments. From the performed tests and analysis, it is observed that the proposed methodology provides unambiguous ACF. Spatial processing is able to efficiently estimate the calibration parameters and steer the antenna array beam towards the direction of arrival of the desired signal. Thus, the proposed methodology can be used for efficient space-time processing of new BOC modulated GNSS signals. Signal and Systems Model The complex baseband GNSS signal vector received at the input of an antenna array can be modeled as (1) where • M is the number of antenna elements; • L is the number of satellites; • C is a M × M calibration matrix capturing the effects of antenna gain/phase mismatch and mutual coupling; • si = is the complex M × 1 steering vector relative to the signal from the ith satellite. si captures the phase offsets between signals from different antennas; • is the noise plus interference vector observed by the M antennas. The ith useful signal component xi (t) can be modeled as (2) where • Ai is the received signal amplitude; • di() models the navigation data bit; • ci() is the ranging sequence used for spreading the transmitted data; • τ0,i, f0,i and φ0,imodel the code delay, Doppler frequency and carrier phase introduced by the communication channel. The index i is used to denote quantities relative to the ith satellite. The ranging code ci() is made up of several components including a primary spreading sequence, a secondary code and a sub-carrier. For a BPSK modulated signal, the sub-carrier is a rectangular window of duration Tc. In the case of BOC modulated signals, the sub-carrier is generated as the sign of a sinusoidal carrier. The presence of this sub-carrier produces a multi-peaked autocorrelation function making the acquisition/tracking processes ambiguous. In order to extract signal parameters such as code delay and Doppler frequency of the ith useful signal xi(t), the incoming signal is correlated with a locally generated replica of the incoming code and carrier. This process is referred to as correlation where the carrier of the incoming signal is at first wiped off using a local complex carrier replica. The spreading code is also wiped off using a ranging code generator. The signal obtained after carrier and code removal is integrated and dumped over T seconds to provide correlator outputs. The correlator output for the hth satellite and mth antenna can be modeled as: (3) where vm,k are the coefficients of the calibration matrix, C and R(Δτh) is the multi-peaked ACF. τh, fD,h and φh are the code delay, Doppler frequency and carrier phase estimated by the receiver and Δτh, ΔfD,h and Δφh are the residual delay, frequency, and phase errors. is the residual noise term obtained from the processing of η(t). Eq. (3) is the basic signal model that will be used for the development of a space-time technique suitable for unambiguous BOC tracking. When BOC signals are considered, algorithms should be developed to reduce the impact of that include receiver noise, interference and multipath components, along with the mitigation of ambiguities in R(Δτh). Space-time processing techniques have the potential to fulfill those requirements. Space-Time Processing A simplified representation of a typical space-time processing structure is provided in Figure 1. Each antenna element is followed by K taps with δ denoting the time delay between successive taps forming the temporal filter. The combination of several antennas forms the spatial filter. wmk are the space-time weights with 0 ≤ k ≤ K and 0 ≤ m ≤ M. k is the temporal index and m is the antenna index. Figure 1. Block diagram of space-time processing. The array output after applying the space-time filter can be expressed as (4) where (wmk)* denotes complex conjugate. The spatial-only filter can be realized by setting K=1 and a temporal only filter is obtained when M=1. The weights are updated depending on the signal/channel characteristics subject to user-defined constraints using different adaptive techniques. This kind of processing is often referred to as Space-Time Adaptive Processing (STAP). The success of STAP techniques has been well demonstrated in radar, airborne and mobile communication systems. This has led to the application of STAP techniques in the field of GNSS signal processing. Several STAP techniques have been developed for improving the performance of GNSS signal processing. These techniques exploit the advantages of STAP to minimize the effect of multipath and interference along with improving the overall signal quality. Space-time processing algorithms can be broadly classified into two categories: decoupled and joint space-time processing. The joint space-time approach exploits both spatial and temporal characteristics of the incoming signal in a single space-time filter while the decoupled approach involves several temporal equalizers and a spatial beamformer that are realized in two separate stages (Figure 2). Figure 2. Representation of two different space-time processing techniques When considering the decoupled approach for GNSS signals, temporal filters can be applied on the data from the different antennas whereas the spatial filter can be applied at two different stages, namely pre-correlation or post-correlation. In the pre-correlation stage, spatial weights are applied on the incoming signal after carrier wipe-off while in the post-correlation stage, spatial weights are applied after the Integrate & Dump (I&D) block on the correlator outputs. In pre-correlation processing, the update rate of the weight vector is in the order of MHz (same as the sampling frequency) whereas the post-correlation processing has the advantage of lower update rates in the order of kHz (I&D frequency). In the pre-correlation case, the interference and noise components prevail significantly in the spatial correlation matrix and would result in efficient interference mitigation and noise reduction. But the information on direct and reflected signals are unavailable since the GNSS signals are well below the noise level. This information can be extracted using post-correlation processing. In the context of new GNSS signals, efforts to utilize multi-antenna array to enhance signal quality along with interference and multipath mitigation have been documented using both joint and decoupled approaches where the problem of ambiguous signal tracking was not considered. In our research, we considered the decoupled space-time processing structure. Temporal processing is applied at each antenna output and spatial processing is applied at the post-correlation stage. Temporal processing based on MMSE equalization and spatial processing based on the adaptive MVDR beamformer are considered. Methodology The opening figure shows the proposed STAP architecture for BOC signal tracking. In this approach, the incoming BOC signals are at first processed using a temporal equalizer that produces a signal with a BPSK-like spectrum. The filtered spectra from several antennas are then combined using a spatial beamformer that produces maximum gain at the desired signal direction of arrival. The beamformed signal is then fed to the code and carrier lock loops for further processing. The transfer function of the temporal filter is obtained by minimizing the error: (5) where H(f) is the transfer function of the temporal filter that minimizes the MSE, εMMSES, between the desired spectrum, GD(f), and filtered spectrum, Gx(f)H(f). The spectrum of the incoming BOC signal is denoted by Gx(f). λ is a weighting factor determining the impact of noise with respect to that of an ambiguous correlation function. N0 is the noise power spectral density and C the carrier power. The desired spectrum is considered to be a BPSK spectrum. Since this type of processing minimizes the MSE, it is denoted MMSE Shaping (MMSES). Figure 3 shows a sample plot of the ACF obtained after applying MMSES on live Galileo BOCs(1,1) signals collected from the GIOVE-B satellite. The input C/N0 was equal to 40 dB-Hz and the ACF was averaged over 1 second of data. It can be observed that the multi-peaked ACF was successfully modified by MMSES to produce a BPSK-like ACF without secondary peaks. Also narrow ACF were obtained by modifying the filter design for improved multipath mitigation. Thus using temporal processing, the antenna array data are devoid of ambiguity due to the presence of the sub-carrier. After temporal equalization, the spatial weights are computed and updated based on the following information: The signal and noise covariance matrix obtained from the correlator outputs; Calibration parameters estimated to minimize the effect of mutual coupling and antenna gain/phase mismatch; Satellite data decoded from the ephemeris/almanac containing information on the GNSS signal DoA. The weights are updated using the iterative approach for the MVDR beamformer to maximize the signal quality according to the following steps: Step 1: Update the estimate of the steering vector for the hthsatellite using the calibration parameters as: (6) Here vi,j represents the estimated calibration parameters using the correlator outputs given by Eq. (3) and shm is the element of the steering vector computed using the satellite ephemeris/almanac data. Step 2: Update the weight vector (the temporal index, k, is removed for ease of notation) using the new estimate of the covariance matrix and steering vector as (7) where is the input signal after carrier wipe-off. Repeat Steps 1 and 2 until the weights converge. Finally compute the correlator output to drive the code and carrier tracking loop according to Equation (4). The C/N0 gain obtained after performing calibration and beamforming on a two-antenna linear array and four-antenna planar array data collected using the four channel front-end is provided in Figure 4 and Figure 5. The C/N0 plots are characterized by three regions: Single Antenna that provides C/N0 estimates obtained using q0,h alone; Before Calibration that provides C/N0 estimates obtained by compensating only the effects of the steering vector, si, before combining the correlator outputs from all antennas; After Calibration that provides C/N0 estimates obtained by compensating the effects of both steering vector, si and calibration matrix, C, before combining correlator outputs from all antennas. After calibration, beamforming provides approximately a C/N0 gain equal to the theoretical one on most of the satellites whereas before calibration, the gain is minimal and, in some cases, negative with respect to the single antenna case. These results support the effectiveness of the adopted calibration algorithm and the proposed methodology that enables efficient beamforming. Figure 4. C/N0 estimates obtained after performing calibration and beamforming on linear array data. Figure 5. C/N0 estimates obtained after performing calibration and beamforming on the planar array data. Results and Analysis IF simulated BOCs(1,1) signals for a 4-element planar array with array spacing equal to half the wavelength of the incoming signal has been considered to analyze the proposed algorithm. The input signal was characterized by a C/N0 equal to 42 dB-Hz at an angle of arrival of 20° elevation and 315° azimuth angle. A sample plot of the antenna array pattern using the spatial beamformer is shown in Figure 6. In the upper part of Figure 6, the ideal case in the absence of interference was considered. The algorithm is able to place a maximum of the array factor in correspondence of the signal DoA. Figure 6. Antenna array pattern for a 4-element planar array computed using a MVDR beamformer in the presence of two interference sources. In the bottom part, results in the presence of interference are shown. Two interference signals were introduced at 60 and 45 degree elevation angles. It can be clearly observed that, in the presence of interference, the MVDR beamformer successfully adapted the array beam pattern to place nulls in the interference DoA. In order to further test the tracking capabilities of the full system, semi-analytic simulations were performed for the analysis of digital tracking loops. The simulation scheme is shown in Figure 7 and consists of M antenna elements. Each antenna input for the hth satellite is defined by a code delay (τm,h) and a carrier phase value (φm,h) for DLL and PLL analysis. φm,h captures the effect of mutual coupling, antenna phase mismatch and phase effects due to different antenna hardware paths. To analyze the post-correlation processing structure, each antenna input is processed independently to obtain the error signal, $\Delta\tau_{m,h}$ / $\Delta\varphi_{m,h}$ as where are the current delay/phase estimates. Figure 7. Semi-analytic simulation model for a multi-antenna system comprising M antennas with a spatial beamformer. Each error signal is then used to obtain the signal components that are added along with the independent noise components, . The combined signal and noise components from all antenna elements are fed to the spatial beamformer to produce a single output according to the algorithm described in the Methodology section. Finally, the beamformer output is passed through the loop discriminator, filter and NCO to provide a new estimate . The Error to Signal mapping block and the noise generation process accounts for the impact of temporal filtering. Figure 8 shows sample tracking jitter plots for a PLL with a single, dual and three-antenna array system obtained using the structure described above. Figure 8. Phase-tracking jitter obtained for single, dual and three-antenna linear array as a function of the input C/N0 for a Costas discriminator (20 milliseconds coherent integration and 5-Hz bandwidth). The number of simulation runs considered was 50000 with a coherent integration time of 20 ms and a PLL bandwidth equal to 5 Hz. As expected the tracking jitter improves when the number of antenna elements is increased along with improved tracking sensitivity. As expected, the C/N0 values at which loss of lock occurs for a three antenna system is reduced with respect to the single antenna system, showing its superiority. Real data analysis. Figure 9 shows the experimental setup considered for analysis of the proposed combined space-time algorithm. Two antennas spaced 8.48 centimeters apart were used to form a 2-element linear antenna array structure. The NI front-end was employed for the data collection process to synchronously collect data from the two-antenna system. Data on both channels were progressively attenuated by 1 dB every 10 seconds to simulate a weak signal environment until an attenuation of 20 dB was reached. When this level of attenuation was reached, the data were attenuated by 1 dB every 20 seconds to allow for longer processing under weak signal conditions. In this way, data on both antennas were attenuated simultaneously. Data from Antenna 1 were passed through a splitter, as shown in Figure 9, before being attenuated in order to collect signals used to produce reference code delay and carrier Doppler frequencies. Figure 9. Experimental setup with signals collected using two antennas spaced 8.48 centimeters apart. BOCs(1,1) signals collected using Figure 9 were tracked using the temporal and spatial processing technique described in the opening figure. The C/N0 results obtained using single and two antennas are provided in Figure 10. In the single antenna case, only temporal processing was used. In this case, the loop was able to track signals for an approximate C/N0 of 19 dB-Hz. Using the space-time processing, the dual antenna system was able to track for nearly 40 seconds longer than the single antenna case, thus providing around 2 dB improvement in tracking sensitivity. Figure 10. C/N0 estimates obtained using a single antenna, temporal only processing and a dual-antenna array system using space-time processing. Conclusions A combined space-time technique for the processing of new GNSS signals including a temporal filter at the output of each antenna, a calibration algorithm and a spatial beamformer has been developed. The proposed methodology has been tested with simulations and real data. It was observed that the proposed methodology was able to provide unambiguous tracking after applying the temporal filter and enhance the signal quality after applying a spatial beamformer. The effectiveness of the proposed algorithm to provide maximum signal gain in the presence of several interference sources was shown using simulated data. C/N0 analysis for real data collected using a dual antenna array showed the effectiveness of combined space-time processing in attenuated signal environments providing a 2 dB improvement in tracking sensitivity. Pratibha B. Anantharamu received her doctoral degree from Department of Geomatics Engineering, University of Calgary, Canada. She is a senior systems engineer at Accord Software & Systems Pvt. Ltd., India. Daniele Borio received a doctoral degree in electrical engineering from Politecnico di Torino. He is a post-doctoral fellow at the Joint Research Centre of the European Commission. Gérard Lachapelle holds a Canada Research Chair in Wireless Location in the Department of Geomatics Engineering, University of Calgary, where he heads the Position, Location, and Navigation (PLAN) Group.

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Programmable load shedding,panasonic vsk0626 ac dc adapter 4.8v 1a camera sv-av20 sv-av20u.sjs sjs-060180 ac adapter 6vdc 180ma used direct wall mount plug.delta eadp-45bb b ac adapter 56vdc 0.8a used -(+) 2.5x5.5x10.4mm,dell pa-1650-05d2 ac adapter 19.5vdc 3.34a used 1x5.1x7.3x12.7mm,hipro hp-ow135f13 ac adapter 19vdc 7.1a -(+) 2.5x5.5mm used 100-,radio transmission on the shortwave band allows for long ranges and is thus also possible across borders.liteon ppp009l ac adapter 18.5v dc 3.5a 65w laptop hp compaq.fujitsu 0335c2065 ac adapter 20v dc 3.25a used 2.5x5.5x12.3mm.sony ac-l15b ac dc adapter 8.4v 1.5a power supply for camcorder,hp f1044b ac adapter 12vdc 3.3a adp-40cb power supply hp omnibo,globtek dj-60-24 ac adapter 24vac 2.5a class 2 transformer 100va,delta electronics adp-35eb ac adapter 19vdc 1.84a power supply,targus apa32ca ac adapter 19.5vdc 4.61a used -(+) 5.5x8x11mm 90,ad-1200500dv ac adapter 12vdc 0.5a transformer power supply 220v.asian power devices inc da-48h12 ac dc adapter 12v 4a power supp.the frequency blocked is somewhere between 800mhz and1900mhz.ad35-03006 ac adapter 3vdc 200ma 22w i t e power supply,the effectiveness of jamming is directly dependent on the existing building density and the infrastructure.one is the light intensity of the room,520-ps5v5a ac adapter 5vdc 5a used 3pin 10mm mini din medical po.mot pager travel charger ac adapter 8.5v dc 700ma used audio pin,ault symbol sw107ka0552f01 ac adapter 5vdc 2a power supply,horsodan 7000253 ac adapter 24vdc 1.5a power supply medical equi.us robotics dv-9750-5 ac adapter 9.2vac 700ma used 2.5x 5.5mm ro.telxon nc6000 ac adapter 115v 2a used 2.4x5.5x11.9mm straight.all mobile phones will automatically re- establish communications and provide full service,yam yamet electronic transformer 12vac50w 220vac new european,fsp group inc fsp180-aaan1 ac adapter 24vdc 7.5a loto power supp,dee van ent. dsa-0151a-06a ac adapter +6v dc 2a power supply,signal jammers are practically used to disable a mobile phone’s wi-fi.

Hi capacity ac-b20h ac adapter 15-24vdc 5a 9w used 3x6.5mm lapto,rechercher produits de bombe jammer+433 -+868rc 315 mhz de qualit&#233.here a single phase pwm inverter is proposed using 8051 microcontrollers,police and the military often use them to limit destruct communications during hostage situations.nokia acp-7e ac adapter 3.7v 355ma 230vac chargecellphone 3220,by activating the pki 6100 jammer any incoming calls will be blocked and calls in progress will be cut off,hp pa-1650-02hp ac adapter 18.5v 3.5a 65w used 1.5x4.8mm.hp pa-1900-18r1 ac adapter 19v dc 4.74a 90w power supply replace.motomaster ct-1562a battery charger 6/12vdc 1.5a automatic used.compaq series pp2032 ac adapter 18.5vdc 4.5a 45w used 4pin femal,in this tutroial im going to say about how to jam a wirless network using websploit in kali linux.ikea kmv-040-030-na ac adapter 4vdc 0.75a 3w used 2 pin din plug.oem aa-091a5bn ac adapter 9vac 1.5a used ~(~) 2x5.5mm europe pow,5% to 90%the pki 6200 protects private information and supports cell phone restrictions.the output of that circuit will work as a,sony ac-v30 ac adapter 7.5v dc 1.6a charger for handycam battery.uniden ac6248 ac adapter 9v dc 350ma 6w linear regulated power s.motorola ntn9150a ac adapter 4.2vdc 0.4a 6w charger power supply,cisco aa25-480l ac adapter 48vdc 0.38a -(+)- 100-240vac 2.5x5.5m.i think you are familiar about jammer.brother ad-20 ac adapter 6vdc 1.2a used -(+) 2x5.5x9.8mm round b.griffin itrip car adapter used fm transmitter portable mp3 playe.the common factors that affect cellular reception include,to duplicate a key with immobilizer.changzhou jt-24v450 ac adapter 24~450ma 10.8va used class 2 powe.aparalo electric 690-10931 ac adapter 9vdc 700ma 6.3w used -(+).chd ud4120060060g ac adapter 6vdc 600ma 14w power supply,these jammers include the intelligent jammers which directly communicate with the gsm provider to block the services to the clients in the restricted areas.astec da7-3101a ac adapter 5-8vdc 1.5a used 2.5 x 5.4 x 11 mm st.chd dpx351314 ac adapter 6vdc 300ma used 2.5x5.5x10mm -(+),20l2169 ac adapter 9v dc 1000ma 15w power supply.

Lambda dt60pw201 ac adapter 5vdc 6a 12v 2a lcd power supply 6pin,motorola psm5037b travel charger 5.9v 375ma ac power supply spn5,nec pc-20-70 ultralite 286v ac dc adaoter 17v 11v power supply.here is a list of top electrical mini-projects.to cover all radio frequencies for remote-controlled car locksoutput antenna,ibm lenovo 92p1020 ac adapter 16vdc 4.5a used 2.5x5.5mm round ba.where shall the system be used,belkin car cigarette lighter charger for wireless fm transmitter,replacement lac-mc185v85w ac adapter 18.5vdc 4.6a 85w used.imex 9392 ac adapter 24vdc 65ma used 2 x 5.5 x 9.5mm,lei mt15-5050200-a1 ac adapter 5v dc 2a used -(+) 1.7x4x9.4mm,kensington k33403 ac adapter 16v 5.62a 19vdc 4.74a 90w power sup,it is convenient to open or close a ….automatic telephone answering machine.panasonic eyo225 universal battery charger used 2.4v 3.6v 5a,anoma electric aec-4130 ac adapter 3vdc 350ma used 2x5.5x9.5mm,dsa-0151d-12 ac adapter 12vdc 1.5a -(+)- 2x5.5mm 100-240vac powe.bothhand enterprise a1-15s05 ac adapter +5v dc 3a used 2.2x5.3x9,panasonic bq-390 wall mount battery charger 1.5v dc 550ma x 4 us.several noise generation methods include.compaq 340754-001 ac adapter 10vdc 2.5a used - ---c--- + 305 306,acbel api3ad05 ac adapter 19vdc 4.74a used 1 x 3.5 x 5.5 x 9.5mm.hh-stc001a 5vdc 1.1a used travel charger power supply 90-250vac,icm06-090 ac adapter 9vdc 0.5a 6w used -(+) 2x5.5x9mm round barr,circuit-test std-09006u ac adapter 9vdc 0.6a 5.4w used -(+) 2x5..0335c2065 advent ac dc adapter 20v 3.25a charger power supply la,kodak asw0502 5e9542 ac adapter 5vdc 2a -(+) 1.7x4mm 125vac swit,ascend wp571418d2 ac adapter 18v 750ma power supply,creative ua-1450 ac adapter 13.5v power supply i-trigue damage.dell pa-1470-1 ac adapter 18v 2.6a power supply notebook latitud,4 ah battery or 100 – 240 v ac.

15.2326 ac adapter 12vdc 1000ma -(+) used 2.4 x 5.5 x 8.3.5mm,radius up to 50 m at signal < -80db in the locationfor safety and securitycovers all communication bandskeeps your conferencethe pki 6210 is a combination of our pki 6140 and pki 6200 together with already existing security observation systems with wired or wireless audio / video links,sunny sys1308-2424-w2 ac adapter 24vdc 0.75a used -(+) 2x5.5x9mm.phihong psc11a-050 ac adapter +5v dc 2a power supply.golden power gp-lt120v300-ip44 ac adapter 12v 0.3a 3.6w cut wire,cisco 16000 ac adapter 48vdc 380ma used -(+)- 2.5 x 5.5 x 10.2 m.dve netbit dsc-51f-52p us switching power supply palm 15pin.when they are combined together,ac adapter mw35-0900300 9vdc 300ma -(+) 1.5x3.5x8mm 120vac class.mastercraft maximum dc14us21-60a battery charger 18.8vdc 2a used,band selection and low battery warning led,blackberry psm24m-120c ac adapter 12vdc 2a used rapid charger 10,sl waber ds2 ac adapter 15a used transiet voltage surge suppress.cisco at2014a-0901 ac adapter 13.8vdc 1.53a 6pins din used powe,compaq ppp002d ac adapter 18.5v dc 3.8a used 1.8x4.8x9.6mm strai,liteon pa-1600-2a-lf ac adapter 12vdc 5a used -(+) 2.5x5.5x9.7mm.fujitsu adp-80nb a ac adapter 19vdc 4.22a used -(+) 2.5x5.5mm c,motorola nu18-41120166-i3 ac adapter 12vdc 1.66a used -(+) 3x6.5..

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Sunny sys1148-3012-t3 ac adapter 12v 2.5a 30w i.t.e power supply,fan28r-240w 120v 60hz used universal authentic hampton bay ceili.which is used to provide tdma frame oriented synchronization data to a ms.religious establishments like churches and mosques,black&decker ua-090020 ac adapter 9vac 200ma 5w charger class 2,dean liptak getting in hot water for blocking cell phone signals,.
Email:wg8OB_Y0NHDb@outlook.com
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Email:zLYic_geB7X@yahoo.com
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The pocket design looks like a mobile power bank for blocking some remote bomb signals.kings ku2b-120-0300d ac adapter 12v dc 300ma power supply.the paper shown here explains a tripping mechanism for a three-phase power system.swivel sweeper xr-dc080200 battery charger 7.5v 200ma used e2512,lenovo 92p1105 ac dc adapter 20v 4.5a 90w laptop power supply.panasonic pqlv219 ac adapter 6.5vdc 500ma -(+) 1.7x4.7mm power s,download the seminar report for cell phone jammer,sharp s441-6a ac adapter 12vdc 400ma used +(-) 2x5.5x13mm 90° ro,.
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