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Permanent Link to Higher Timing Accuracy, Lower Cost
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AURORA BOREALIS seen from Churchill, Manitoba, Canada. Ionospheric scintillation research can benefit from this new method. (Photo: Aiden Morrison) Photo: Canadian Armed Forces By Aiden Morrison, University of Calgary Two broad user groups will find important consequences in this article: Time synchronization and test equipment manufacturers, whose GPS-disciplined oscillators have excellent long-term performance but short- to medium-term behavior limited by the quality, and therefore cost, of the integrated quartz device. This article portends a family of devices delivering oven-controlled crystal oscillator (OCXO) performance down to the 10-millisecond level, with an oscillator costing pennies, rather than tens or hundreds of dollars. Applications include ionospheric scintillation research (above). High-performance receiver manufacturers who design products for high-dynamic or high-vibration environments (see cover) where the contribution of phase noise from the local oscillator to velocity error cannot be ignored. In these areas, the strategy outlined here would produce equipment that can perform to higher specifications with the same or a lower-cost oscillator. The trade-off requires two tracking channels per satellite signal, but this should not pose a problem. At ION GNSS 2009, manufacturers showed receivers with 226 tracking channels. There are currently only 75 live signals in the sky, including all of GPSL1/L2/L5 and GLONASS L1/L2. — Gérard Lachapelle If the channel data within a GNSS receiver is handled in an effective manner, it is possible to form meaningful estimates of the local-oscillator phase deviations on timescales of 10 milliseconds (ms) or less. Moreover, if certain criteria are met, these estimates will be available with related uncertainties similar to the deviations produced by a typical oven-controlled crystal oscillator (OCXO). The processing delay required to form this estimate is limited to between 10 and 20 ms. In short, it becomes possible in near-real-time to remove the majority of the phase noise of a local oscillator that possesses short-term instability worse than an OCXO, using standalone GNSS. This represents both a new method to accurately determine

the Allan deviation of a local oscillator at time scales previously impractical to assess using a conventional GNSS receiver, and the potential for the reduction in observable Doppler uncertainty at the output of the receiver, as well as ionospheric scintillation detection not reliant on an expensive local OCXO. Concept. Inside a typical GNSS receiver, the estimate of the error in the local oscillator is formed as a component of the navigation solution, which is in turn based on the output of each satellite-tracking channel propagating its estimate of carrier and code measurements to a common future point. While this method of ensuring simultaneous measurements is necessary, it regrettably limits the resolution with which the noise of the local oscillator can be quantified, due to the scaling of non-simultaneous samples of local oscillator noise through the measurement propagation process. To bypass these shortcomings requires a method of coherently gathering information about the phase change in the local oscillator across all available satellite signals: to use the same samples simultaneously for all satellites in view to estimate the center-point phase error common across the visible constellation. To explain how this is feasible, we must first understand the limitations imposed by the conventional receiver architecture, with respect to accurately estimating short-term oscillator behavior, and subsequently to determine the potential pitfalls of the proposed modifications, including processing delays needed for bit wipe-off, expected observation noise, and user dynamics effects. Typical Receiver Shortfalls In a typical receiver, while information about local time offset and local oscillator frequency bias may be recovered, information about phase noise in the local oscillator is distorted and discarded, as a consequence of scaling non-simultaneous observations to a common epoch. As shown in FIGURE 1, coherent summation intervals in a receiver are used to approximate values of the phase error, including oscillator phase, measured at the non-simultaneous interval centrers in each channel, which are then propagated to a common navigation solution epoch. Each channel will intrinsically contain a partially overlapping midpoint estimate of oscillator noise over the coherent summation interval that will then be scaled by the process of extrapolation. As these estimates are scaled and partially overlapping, they do not make optimal use of the information known about the effects of the local oscillator, and form a poor basis for estimating the contributions of this device to the uncertainty in the channel measurements. As shown in Figure 1, the phase error measured in each channel will be distorted by an over unity scaling factor. FIGURE 1. Propagation and scaling of phase estimates withina typical receiver. Depending on implementation decisions made by the designers of a given GNSS system, the average value of the propagation interval relative to the bit period will have different expected values. Assuming the destination epoch is the immediate end of the furthest advanced (most delayed) satellite bitstream, and that integration is carried out over full bit periods, the minimum propagation interval for this satellite would be ½-bit period. For the average satellite however, the propagation delay would be this ½-bit period plus the mean skew between the furthest satellite and the bitstreams of other space vehicles. Ignoring further skew effects due to the clock errors within the satellites, which are typically limited well below the ms level, the skew between highest and lowest elevation GPS satellites for a user on the surface of earth would be approximately 10 ms. The average value of this skew due to ranging change over orbit, assuming an even distribution of satellites in the sky at different elevation angles, would therefore be 5 ms. Combining the minimum value of the skew interval with the minimum propagation interval of the most delayed satellite yields a total average propagation interval of 15 ms. In turn, this gives a typical scaling factor of 1.75, used from this point forward when referring to the effects of scaling this quantity. Proposed Implementation Overcoming limitations of a typical receiver requires recording the approximate bit-timing and history of each tracked satellite as well as a short segment of past samples. This retained data guarantees that the bit-period boundaries of the satellites will not pose an obstacle to forming common N-ms coherent periods between all visible satellites, over which simultaneous integration may proceed by wiping off bit transitions. Using this approach as shown in FIGURE 2, all available constellation signal power is used to estimate a single parameter, namely the epoch-to-epoch phase change in the local oscillator. FIGURE 2. Common intervals over which to accurately estimate local oscillator phase changes. Having viewed the existence of these common periods, it becomes evident that it is conceptually possible to form time-synchronized estimates of the phase contribution of the common system oscillator alternately across one N-ms time slice, then the next, in turn forming an unb roken time series of estimates of the phase change of the system oscillator. Forming the difference between the adjacent discriminator outputs will provide the following information: The ΔEps (change in the noise term in the local loop) The ΔOsc (change in the phase of the local oscillator, the parameter of interest) The ΔDyn (change in the untracked/residual of real and apparent dynamics of the local loop/estimator) Noticing that term 1 may be considered entirely independent across independent PRNs (GPS, Galileo, Compass) or frequency channels (GLONASS), and that the value of term 3 over a 10-ms period is expected to be small over these short intervals, it becomes obvious that term 2 can be recovered from the available information. To determine the weighting for each satellite channel, the variance of the output of the discriminator is needed. Performance Determination To allow the realistic weighting of discriminator output deltas, it becomes desirable to estimate at very short time intervals the variance of the output of the phase discriminator. In the case of a 2-quadrant arctangent discriminator, this means one wishes to quantify the variance Letting Q/I 5 Z, recall that if Y 5 aX then Applying this to the variance of the input to the arctangent discriminator in terms of the in phase and quadrature accumulators, this would give Rather than proceed with a direct evaluation from this point onward to determine the expression for the variance at the output of the discriminator, it is convenient to recognize that simpler alternatives exist since The implication is that since the slope of the arctangent transfer function is very nearly equal to 1 in the central, typical operating region, and universally less than 1 outside of this region, it is easy to recognize that the variance at the output of the arctangent discriminator is universally less than that at the input, and can be pessimistically quantified as the variance of the input, or σ2(Z). This assumption has been verified by simulation, its result shown in FIGURE 3, where the response has been shown after taking into account the effect of operating at a point anywhere in the range ±45 degrees. While the consequence of the simplification of the variance expression is an exaggeration of discriminator output variance, FIGURE 4 shows output variance is well bounded by the estimate, and within a small margin of error for strong signals. FIGURE 3. Predicted variances at the output of the ATAN2discriminator versus C/N0. FIGURE 4. Difference between actual and predicted variance at output of discriminator. The gap between real and predicted output variance may also be narrowed in cases where Q>I by using a type of discriminator which interchanges Q and I in this case and adds an appropriate angular offset to the output as Proceeding in this vein, the next required parameter is the normalized variance of the in-phase and quadrature arms. The carrier amplitude A can be roughly approximated as Resulting in a carrier power C Further, the noise power is given as Expressing bandwidth B as the inverse of the coherent integration time, and rearranging now gives noise density N0 as Combining this expression, and the one previously given for the carrier power C results in the following expression for the carrier to noise density ratio: This latest expression can be rearranged to find the desired variance term. Assuming the 10-ms coherent integration time discussed earlier is used, this yields Normalizing for the carrier amplitude gives the normalized variance in terms of radians squared: In any situation where the carrier is sufficiently strong to be tracked, it is likely that the carrier power term employed above can be gathered from the immediate I and Q values, ignoring the contribution of the noise term to its magnitude. Oscillator Phase Effect. Determining the expected magnitude of the local oscillator phase deviation requires only three steps, assuming that certain criteria can be met. The first requirement is that the averaging times in question must be short relative to the duration, at which processes other than white phase and flicker phase modulation begin to dominate the noise characteristics of the oscillator. Typically the crossover point between the dominance of these processes and others is above 1 s in averaging interval length, when quartz oscillators are concerned. Since this article discusses a specific implementation interval of 10 ms within systems expected to be using quartz oscillators, it is reasonable to assume that this constraint will be met. The second requirement is that the Allan deviation of the given system oscillator must be known for at least one averaging interval within the region of interest. Since the Allan deviation follows a linear slope of -1 with respect to averaging interval on a log-log scale within the white-phase noise region, this single value will allow an accurate prediction of the Allan deviation at any other point on the interval and, in turn, of the phase uncertainty at the 10 ms averaging interval level. Letting σΔ(τ) represent the Allan deviation at a specific averaging interval, recall that this quantity is the midpoint average of the standard deviation of fractional frequency error over the averaging interval τ. Scaling this quantity by a frequency of interest results in the standard deviation of the absolute frequency error on the averaging interval: By integrating this average difference in frequency deviations over the coherent period of interest, one obtains a measure of the standard deviation in degrees, of a signal generated by this reference: Note that the averaging interval τ must be identical to the coherent integration time. Turning to a practical example, if the oscillator in question has a 1 s Allan Deviation of 1 part per hundred billion (1 in 1011), a stability value between that of an OCXO and microcomputer compensated crystal oscillator (MCXO) standard, and shown to be somewhat pessimistic, this would scale linearly to be 1e-9 at a 10-ms averaging interval, under the previous assumption that the oscillator uncertainty is dominated by the white phase-noise term at these intervals. Also, for illustration purposes, if one assumes the carrier of interest to be the nominal GPS L1 carrier, the uncertainty in the local carrier replica due to the local oscillator over a 10-ms coherent integration time becomes When stated in a more readily digested format, this represents roughly 15 centimeter/second in the line-of-sight velocity uncertainty. In an operating receiver, two additional factors modify this effect. The first is the previously discussed scaling effect that will tend to exaggerate this effect by a typical factor of 1.75, as previously discussed. The second factor is that this noise contribution is filtered by the bandwidth-limiting effects of the local loop filter, producing a modification to the noise affecting velocity estimates, as well as reduced information about the behaviour of the local oscillator. Impact of Apparent Dynamics. When considering the error sources within the system, it is important to realize which individual sources of error will contribute to estimation errors, and which will not. One area of potential concern would appear to be the errors in the satellite ephemerides, encompassing both the satellite-orbit trajectory misrepresentation and the satellite clock error. While the errors in the satellite ephemerides are of concern for point positioning, they are not of consequence to this application, as the apparent error introduced by a deviation of the true orbit from that expressed in the broadcast orbital parameters does not affect the tracking of that satellite at the loop level. Additionally, while the satellite clock will add uncertainty to the epoch-to-epoch phase change within each channel independently, the magnitude of this change is minimal relative to the contribution of uncertainty due to the variance at the output of the discriminator guaranteed by the low carrier-to-noise density ratio of a received GNSS signal. Since this contribution is uncorrelated between satellites and relatively small compared to other noise contributions affecting these measurements, even when compared to the soon-to-be-discontinued Uragan GLONASS satellites that had generally less stable onboard clocks, it is likely safe to ignore. When compared to the more stable oscillators aboard GPS or GLONASS-M satellites, it is a reasonable assumption that this will be a dismissible contribution to received signal-phase uncertainty change. While atmospheric effects present an obstacle which will directly affect the epoch-to-epoch output of the discriminators, it is believed that under conditions that do not include the effects of ionospheric scintillation the majority of the contribution of apparent dynamics due to atmospheric changes will have a power spectral density (PSD) heavily concentrated below a fraction of 1 Hz. The consequence of this concentration is that the tracking loops will remove the vast majority of this contribution, and that the difference operator that will be applied between adjacent phase measurements, as in the case of dynamics, will nullify the majority of the remaining influence. Impact of Real Dynamics. Real dynamics present constraints on performance, as do any tracking loop transients. For example, a low-bandwidth loop-tracking dynamics will have long-lasting transients of a magnitude significant relative to levels of local oscillator noise. For this reason it is necessary to adopt a strategy of using the epoch-to-epoch change in the discriminator as the figure of interest, as opposed to the absolute error-value output at each epoch. This can reasonably be expected to remove the vast majority of the effects of dynamics of the user on the solution. To validate this assumption under typical conditions calls for a short verification example. Assuming the use of a second-order phase-locked loop (PLL) for carrier tracking, with a 10-Hz loop bandwidth the effects of dynamics on the loop are given by these equations: Letting Bn be 10 Hz, one can write Recall that the dynamic tracking error in a second-order tracking loop is given by Given the choices above, this would result in a constant offset of 0.00281 cycles, or 1.011 degrees of constant tracking error due to dynamics, following from the relation between line-of-sight acceleration and loop bandwidth to tracking error. Since this constant bias will be eliminated by the difference operator discussed earlier, it is necessary to examine higher order dynamics. Further, if one used a coherent integration interval of 10 ms as assumed earlier, and let the dynamics of interest be a jerk of 1 g/s, this results in a midpoint average of 0.005 g on this interval: Substituting this result into equation 16 produces the associated change in dynamic error over the integration interval, which is in this case: This value will be kept in mind when evaluating capabilities of the estimation approach to determine when it will be of consequence. As the estimation process will be run after a short delay, an existing estimate of platform dynamics could form the basis of a smoothing strategy to reduce this dynamic contribution further. Estimated Capabilities In the absence of the influence of any unmodeled effects, the expected performance of this method is dependent on only the number of satellite observables and their respective C/N0 ratios. Across each of these scenarios we assume for simplicity’s sake that each satellite in view is received at a common C/N0 ratio and over a common integration period of 10 ms. If the assumption of minimal dynamic influences is met, the situation at hand becomes one in which multiple measures of a single quantity are present, each containing independent (due to CDMA or FDMA channel separation) noise influences with a nearly zero mean. When one can express the available data form: x[n] = R + w[n] where x[n] is the nth channel discriminator delta which includes the desired measure of the local oscillator delta (R), as well as w[n], a strong, nearly white-noise component, there are multiple approaches for the estimation of R. The straightforward solution to estimate R in this case is to use the predicted variances of each measure to serve as an inverse weighting to the contribution of each individual term, followed by normalization by the total variance, as expressed by Now, since it is desired to bound the uncertainty of the estimate of R, the variance of this quantity should also be noted. This uncertainty can be determined as To determine the performance of the estimation method for a given constellation configuration, with specific power levels and available carrier signals, it is necessary to utilize the predicted variances plotted in Figure 3 as inputs to equations 20 and 21. To provide numerical examples of the performance of this method, three scenarios span the expected range of performance. Scenario 1 is intended to be char-acteristic of that visible to a single-freq-uency GPS user under slight attenuation. It is assumed that 12 single-frequency satellites are visible at a common C/N0 of 36 dB-Hz, yielding from the simulation curves a value for each channel of 0.0265 rad2. When substituted into equation 24, this predicts an estimation uncertainty of This is a level of estimation uncertainty similar to that assumed to be intrinsic to the local oscillator in the previous section. The result implies that with this minimally powerful set of satellites, it becomes possible to quantify the behavior of the local oscillator with a level of uncertainty commensurate with the actual uncertainty in the oscillator over the 10 ms averaging interval. Consequentially, this indicates that the Allan deviation of this system oscillator could be wholly evaluated under these conditions at any interval of 10 ms or longer. Further, if the system oscillator were in fact the less stable MCXO from the resource above, this estimate uncertainty would be significantly lower than the actual uncertainty intrinsic to the oscillator, providing an opportunity to “clean” the velocity measurements. Scenario 2 is intended to be characteristic of a near future multi-constellation single-frequency receiver. It is assumed that eight satellites from three constellations are visible on a single frequency each, with a common C/N0 of 42 dB-

Hz, yielding a value for each channel of 6.4e-3 rad2, leading to an estimation uncertainty of Scenario 3 is intended to serve as an optimistic scenario involving a future multi-frequency, multi-constellation receiver. It is assumed that nine future satellites are available from each of three constellations, each with four independent carriers, all received at 45 dB-Hz, yielding a value for each channel of 3.2e-3 rad2, leading to an estimation uncertainty of Application to Observations The theoretical benefit of subtracting these phase changes from the measurements of an individual loop prior to propagating that measurement to the common position solution epoch ranges from moderate to very high depending on the satellite timing skew relative to the solution point. The most beneficial scenario is total elimination of oscillator noise effects (within the uncertainty of the estimate), which is experienced in the special case (Case A, FIGURE 5), where the bit period of a given satellite falls entirely over two of the 10-ms subsections. The uncertainty would increase to 2x the level of uncertainty in the estimate in the special case (Case B) where the satellite bit period straddles one full 10-ms period and two 5-ms halves of adjacent periods, and would lie somewhere between 1 and 2 times the level of uncertainty for the general case where three subintervals are covered, yet the bit period is not centered (Case C). FIGURE 5. Special cases of oscillator estimate versus bit-period alignment. While the application to observations of the predicted oscillator phase changes between integration intervals does not appear immediately useful for high-end receiver users with the exception of those in high-vibration or scintillation-detection applications, it could be applied to consumer-grade receivers to facilitate the use of inexpensive system clocks while providing observables with error levels as low as those provided by much more expensive receivers incorporating ovenized frequency references. Further Points While the chosen coherent integration period may be lengthened to increase the certainty of the measurement from a noise averaging perspective, this modification risks degrading the usefulness of said measurement due to dynamics sensitivities. Additionally, as the coherent integration time is increased, the granularity with which the pre-propagation oscillator contribution may be removed from an individual loop will be reduced. While this may be useful in cases of very low dynamics where the system is intended to estimate phase errors in a local oscillator with high certainty, it would be of little use if one desires to provide low-noise observables at the output. For this reason, it is recommended that increases in coherent integration time be approached with caution, and extra thought be given to use of dynamics estimation techniques such as smoothing, via use of the subsequent n-ms segment in the formation of the estimate of dynamics for the “current” segment. This carries the penalty of increased processing latency, but could greatly reduce dynamics effects by enabling their more reliable excision from the desired phase-delta measurements. Acknowledgments The author thanks his supervisors, Gerard Lachapelle and Elizabeth Cannon, and the Natural Sciences and Engineering Research Council of Canada, the Alberta Informatics Circle of Research Excellence, the Canadian Northern Studies Trust, the Association of Canadian Universities for Northern Studies, and Environment Canada for financial and logistical support.
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Apple powerbook duo aa19200 ac adapter 24vdc 1.5a used 3.5 mm si.dell pa-1650-05d2 ac adapter 19.5vdc 3.34a used 1x5.1x7.3x12.7mm,9 v block battery or external adapter,dsc ptc1640 ac adapter 16.5vac 40va used screw terminal power su.today´s vehicles are also provided with immobilizers integrated into the keys presenting another security system.10k2586 ac adapter 9vdc 1000ma used -(+) 2x5.5mm 120vac power su,aps aps40-es-30 ac adapter +5v 6a +12v 1a -12v 0.5a used 5pin.yl5u ac adapter 12vdc 200ma -(+) rf connecter used 0.05x9.4mm.backpack bantam aua-05-1600 ac adapter 5v 1600ma used 1.5 x 4 x,li shin lse9901b1260 ac adapter12vdc 5a 60w used 4pin din power,conair tk952c ac adapter european travel charger power supply.it will be a wifi jammer only,ahead mw41-1200500a ac adapter ac 12v 500ma straight round barre,jvc aa-v68u ac adapter 7.2v dc 0.77a 6.3v 1.8a charger aa-v68 or,the output of each circuit section was tested with the oscilloscope.cisco wa15-050a ac adapter +5vdc 1.25a used -(+) 2.5x5.5x9.4mm r,high voltage generation by using cockcroft-walton multiplier,remember that there are three main important circuits.xings ku1b-038-0080d ac adapter 3.8vdc 80ma used shaverpower s.5% to 90%modeling of the three-phase induction motor using simulink.shenzhen jhs-q05/12-s334 ac adapter 12vdc 5v 2a s15 34w power su.hp 391173-001 ac dc adapter 19v 4.5a pa-1900-08h2 ppp014l-sa pow,due to the high total output power.bellsouth dv-1250 ac adapter 12vdc 500ma power supply.shenzhen rd1200500-c55-8mg ac adapter 12vdc 1a used -(+) 2x5.5x9.noise circuit was tested while the laboratory fan was operational.ryobi 1400656 1412001 14.4v charger 16v 2a for drill battery.if you are in the united states it is highly illegal to own,cwt paa050f ac adapter 12vdc 4.16a used 2.5x5.5mm -(+) 100-240va,remington wdf-6000c shaver base cradle charger charging stand.d-link m1-10s05 ac adapter 5vdc 2a -(+) 2x5.5mm 90° 120vac route,a cell phone jammer is an small equipment that is capable of blocking transmission of signals between cell phone and base station,the pki 6200 features achieve active stripping filters,car adapter charger used 3.5mm mono stereo connector,thermo gastech 49-2163 ac adapter 12.6vdc 220/70ma battery charg,cincon tr100a240 ac adapter 24vdc 4.17a 90degree round barrel 2.,tif 8803 battery charger 110v used 2mm audio pin connector power,zip drive ap05f-us ac adapter 5vdc 1a used -(+) 2.5x5.5mm round,atlinks 5-2418a ac adapter 9vac 400ma ~(~) 2x5.5mm 90° used 120v,apple m3365 ac adapter 13.5vdc 1a -(+) 1x3.4x4.8mm tip 120vac 28,this article shows the different circuits for designing circuits a variable power supply,replacement 65w-ap04 ac adapter 24vdc 2.65a used - ---c--- +,bose s024em1200180 12vdc 1800ma-(+) 2x5.5mm used audio video p.mw48-1351000 ac adapter 13.5vdc 1a used 2 x 5.5 x 11mm,minolta ac-9 ac-9a ac adapter 4.2vdc 1.5a -(+) 1.5x4mm 100-240va,ibm aa19650 ac adapter 16vdc 2.2a class 2 power supply 85g6709.toshiba pa3083u-1aca ac adapter 15vdc 5a used-(+) 3x6..5mm rou,jammer detector is the app that allows you to detect presence of jamming devices around.a1036 ac adapter 24vdc 1.875a 45w apple g4 ibook like new replac.lac-cp19v 120w ac adapter 19v 6.3a replacement power supply comp,here is the project showing radar that can detect the range of an object,liteon pa-1900-24 ac adapter 19v 4.74a acer gateway laptop power.atlinks 5-2495a ac adapter 6vdc 300ma used -(+) 2.5x5.5x12mm rou.sps15-12-1200 ac adapter 12v 1200ma direct plug in power supply.panasonic cf-aa1653 j2 ac adapter

15.6v 5a power supply universa.radioshack 23-240b ac adapter 9.6vdc 60ma used 2-pin connector,please pay special attention here,component telephone u090025a12 ac adapter 9vac 250ma ~(~) 1.3x3.,li shin international enterprise 0322b1224 ac adapter 12vdc 2a u,chd ud4120060060g ac adapter 6vdc 600ma 14w power supply.tdc power da-18-45d-ei35 ac adapter 4.5v 0.4a 1.8va class 2 tran,ilan elec f1700c ac adapter 19v dc 2.6a used 2.7x5.4x10mm 90,automatic telephone answering machine,mei mada-3018-ps ac adapter 5v dc 4a switching power supply,astec sa25-3109 ac adapter 24vdc 1a 24w used -(+) 2.5x5.5x10mm r,a booster is designed to improve your mobile coverage in areas where the signal is weak,lishin lse0202c2090 ac adapter 20v dc 4.5a power supply,as many engineering students are searching for the best electrical projects from the 2nd year and 3rd year,car ac adapter used power supply special phone connector,phihong psa31u-050 ac adapter 5vdc 4a 1.3x3.5mm -(+) used 100-24,an antenna radiates the jamming signal to space,cincon tr513-1a ac adapter 5v 400ma travel charger,creative mae180080ua0 ac adapter 18vac 800ma power supply.sony ac-v35 ac power adapter 7.5vdc 1.6a can use with sony ccd-f,ron gear rgd35-03006 ac adapter 3vdc 300ma used -(+) 0.15x2.5x10.it is also buried under severe distortion.energizer pl-7526 ac adapter6v dc 1a new -(+) 1.5x3.7x7.5mm 90.

Dragon sam-eaa(i) ac adapter 4.6vdc 900ma used usb connector swi,this project shows charging a battery wirelessly,premium power 298239-001 ac adapter 19v 3.42a used 2.5 x 5.4 x 1,sanken seb55n2-16.0f ac adapter 16vdc 2.5a power supply,black & decker vp130 versapack battery charger used interchangea.netgear sal018f1na ac adapter 12vdc 1.5a used -(+) 2x5.5x9mm rou,ad-0815-u8 ac adapter 7.5vdc 150ma used -(+)- 4.5 x 5.6 x 9 mm 2,there are many types of interference signal frequencies,and here are the best laser jammers we’ve tested on the road,panasonic eb-ca10 ac adapter 7vdc 600ma used 1.5 x 3.4 x 9 mm st,basler electric be115230cab0020 ac adapter 5vac 30va a used,this system also records the message if the user wants to leave any message,motorola am509 ac adapter 4.4v dc 1.1 a power supply spn4278d,anoma aec-n35121 ac adapter 12vdc 300ma used -(+) 2x5.5mm round,hp compaq ppp009h ac adapter 18.5vdc 3.5a -(+) 1.7x4.8 100-240va.sony ac-v30 ac adapter 7.5v dc 1.6a charger for handycam battery.armoured systems are available.nokia ac-5e ac adapter cell phone charger 5.0v 800ma euorope ver.fisher price pa-0610-dva ac adapter 6vdc 100ma power supply,energizer pc-1wat ac adapter 5v dc 2.1a usb charger wallmount po.the source ak00g-0500100uu 5816516 ac adapter 5vdc 1a used ite,rocketfish rf-bprac3 ac adapter 15-20v/5a 90w used,dell adp-90fb ac adapter pa-9 20v 4.5a used 4-pin din connector.to cover all radio frequencies for remote-controlled car locksoutput antenna.avaya switcher ii modular base unit with pc port 408012466 new,bionx hp1202l3 01-3444 ac adaptor 37vdc 2a 4pin xlr male used 10.phase sequence checker for three phase supply.it is convenient to open or close a ….nikon eh-69p ac adapter 5vdc 0.55a used usb i.t.e power supply 1.ktec ksafc0500150w1us ac adapter 5vdc 1.5a -(+) 2.1x5.5mm used c.hk-b518-a24 ac adapter 12vdc 1a -(+)- ite power supply 0-1.0a.royal a7400 ac adapter 7vac 400ma used cut wire class 2 power su,car adapter 7.5v dc 600ma for 12v system with negative chassis g,replacement pa-1700-02 ac adapter 20v 4.5a power supply.delta electronics adp-36db rev.a ac power adapter ast laptop.motorola spn5404aac adapter 5vdc 550ma used mini usb cellphone,intermediate frequency(if) section and the radio frequency transmitter module(rft).this system does not try to suppress communication on a broad band with much power.communication can be jammed continuously and completely or.cincon electronics tr36a15-oxf01 ac adapter 15v dc 1.3a power su,dell da65ns3-00 ac adapter 19.5v dc 3.34aa power supply,codex yhp-1640 ac adapter 16.5vac 40va power supply plugin class,toshiba adp-65db ac adapter 19vdc 3.42a 65w for gateway acer lap,us robotics dv-9750-5 ac adapter 9.2vac 700ma used 2.5x 5.5mm ro.here is a list of top electrical mini-projects,beigixing 36vdc 1.6a electric scooter dirt bike razor charger at,cable shoppe inc oh-1048a0602500u-ul ac adapter 6vdc 2.5a used.galaxy sed-power-1a ac adapter 12vdc 1a used -(+) 2x5.5mm 35w ch.how to disable mobile jammer | spr-1 mobile jammer tours replies,delta adp-50gh rev.b ac adapter 12vdc 4.16a used 2 x 5.5 x 9.5mm.motorola psm4841b ac adapter 5.9vdc 350ma cellphone charger like.altec lansing s024eu1300180 ac adapter 13vdc 1800ma -(+) 2x5.5mm,gfp-151da-1212 ac adapter 12vdc 1.25a used -(+)- 2x5.5mm 90° 100,qun xing ac adapter 1000ma used 100vac 2pin molex power supply.ea10362 ac adapter 12vdc 3a used -(+) 2.5x5.5mm round barrel,this project shows the automatic load-shedding process using a microcontroller.toshiba pa3201u-1aca ac adaptor 15v 5a 1800 a50 5005 m5 r200 lap,a&d tb-233 ac adapter 6v dc 500ma used -(+) 2x5.5mm barrel 120va.ault cs240pwrsup ac adapter 7.5vdc 260ma used 9.0vac 250ma,du060030d ac adapter 6vdc 300ma -(+) 1x2.3mm used 120vac class 2,vt070a ac adatper 5vdc 100ma straight round barrel 2.1 x 5.4 x 1,ultra ulac901224ap ac adapter 24vdc 5.5a used -(+)5.5x8mm power,three phase fault analysis with auto reset for temporary fault and trip for permanent fault.this project shows the system for checking the phase of the supply.motorola htn9014c 120v standard charger only no adapter included,starting with induction motors is a very difficult task as they require more current and torque initially.despite the portable size g5 creates very strong output power of 2w and can jam up to 10 mobile phones operating in the neatest area,ault t41-120750-a000g ac adapter 12vac 750ma used ~(~)2.5x5.5,panasonic kx-tca1 ac adapter 9vdc 350ma +(-) 2x5.5mm used cordle,when the temperature rises more than a threshold value this system automatically switches on the fan.edacpower ea10953 ac adapter 24vdc 4.75a -(+) 2.5x5.5mm 100-240v.520-ntps12 medical power source12vdc 2a used 3pin male adapter p,sceptre power s024em2400100 ac adapter 24vdc 1000ma used -(+) 1.,au41-160a-025 ac adapter 16vac 250ma used ~(~) 2.5x5.5mm switch,the same model theme as the weboost.depending on the vehicle manufacturer,toshiba pa2426u ac adapter 15vdc 1.4a used -(+) 3x6.5mm straight.

Gpe gpe-828c ac adapter 5vdc 1000ma used -(+) 2.5x5.5x9.4mm 90°,samsung atadv10jbe ac adapter 5v dc 0.7a charger cellphone power.phihong psaa18u-120 ac adapter 12vdc 1500ma used +(-) 2x5.5x12mm.whether copying the transponder.the civilian applications were apparent with growing public resentment over usage of mobile phones in public areas on the rise and reckless invasion of privacy,hp hstn-f02x 5v dc 2a battery charger ipaq rz1700 rx,ibm 35g4796 thinkpad ac dc adapter 20v dc 700 series laptop pow.variable power supply circuits.350901002coa ac adapter 9vdc 100ma used -(+)-straight round ba,compaq up04012010 ac adapter 5v 2a 12v 2.3a laptop lcd power sup.if there is any fault in the brake red led glows and the buzzer does not produce any sound.spectralink ptc300 trickle 2.0 battery charger used for pts330 p,this multi-carrier solution offers up to ….apple m7332 ac adapter 24vdc 1.875a 2.5mm 100-240vac 45w ibook g,ibm 92p1016 ac adapter 16v dc 4.5a power supply for thinkpad,hp f1044b ac adapter 12vdc 3.3a adp-40cb power supply hp omnibo.intertek bhy481351000u ac adapter 13.5vdc 1000ma used -(+) 2.3x5,sony cechza1 ac adapter 5vdc 500ma used ite power supply 100-240,lp-60w universal adapter power supply toshiba laptop europe,dve dsa-0421s-12330 ac adapter 13v 3.8a switching power supply,wacom aec-3512b class 2 transformer ac adatper 12vdc 200ma strai,nikon eh-5 ac adapter 9vdc 4.5a switching power supply digital c.ibm 02k7006 ac adapter 16vdc 3.36a used -(+)- 2.5x5.5mm 100-240v,jamming these transmission paths with the usual jammers is only feasible for limited areas.outputs obtained are speed and electromagnetic torque.delta electronics adp-35eb ac adapter 19vdc 1.84a power supply,nokia acp-7e ac adapter 3.7v 355ma 230vac chargecellphone 3220.apple a1172 ac adapter 18vdc 4.6a 16vdc 3.6a used 5 pin magnetic,khu045030d-2 ac adapter 4.5vdc 300ma used shaver power supply 12,th 5vdc 11v used travel charger power supply 90-250vac phone,hp compaq adp-65hb b ac adapter 18.5vdc 3.5a -(+) 1.7x4.8mm used.viasys healthcare 18274-001 ac adapter 17.2vdc 1.5a -(+) 2.5x5.5,950-950015 ac adapter 8.5v 1a power supply,altas a-pa-1260315u ac adapter 15vdc 250ma -(+) 0.6x9.5 rf used,illum fx fsy050250uu0l-6 ac adapter 5vdc 2.5a used -(+) 1x3.5x9m.globtek gt-4076-0609 ac adapter 9vdc 0.66a -(+)- used 2.6 x 5.5,northern telecom ault nps 50220-07 l15 ac adapter 48vdc 1.25a me,10 and set the subnet mask 255,ibm 85g6733 ac adapter 16vdc 2.2a 4 pin power supply laptop 704.jhs-q05/12-334 ac adapter 5vdc 2a usedite power supply 100-240.dve dsa-0051-05 fus 55050 ac adapter 5.5vdc .5a usb power supply,goldfear ac adapter 6v 500ma cellphone power supply.3m 521-01-43 ac adapter 8.5v 470ma used - working 3 pin plug cla,3 w output powergsm 935 – 960 mhz,2 w output powerphs 1900 – 1915 mhz,replacement seb100p2-15.0 ac adapter 15vdc 8a 4pin used pa3507u-.audiovox 28-d12-100 ac adapter 12vdc 100ma power supply stereo m.5810703 (ap2919) ac adapter 5vdc 1.5a -(+) used 1.5x4x10 mm 90°.delta sadp-65kb d ac adapter 19v dc 3.42a used 2.3x5.5x9.7mm.i think you are familiar about jammer,15.2326 ac adapter 12vdc 1000ma -(+) used 2.4 x 5.5 x 8.3.5mm.sony ac-64n ac adapter 6vdc 500ma used -(+) 1.5x4x9.4mm round ba,new bright a519201194 battery charger 7v 150ma 6v nicd rechargab.kodak k4500 ni-mh rapid battery charger2.4vdc 1.2a wall plug-i,tpi tsa1-050120wa5 ac dc adapter 5v 1.2a charger class 2 power s.universal 70w-a ac adapter 12vdc used 2.4 x 5.4 x 12.6mm detacha.compaq pe2004 ac adapter 15v 2.6a used 2.1 x 5 x 11 mm 90 degree,dell adp-50sb ac adapter 19vdc 2.64a 2pin laptop power supply.delphi sa10115 xm satellite radio dock cradle charger used 5vdc,371415-11 ac adapter 13vdc 260ma used -(+) 2x5.5mm 120vac 90° de,helps you locate your nearest pharmacy.apple usb charger for usb devices with usb i pod charger.duracell cefadpus 12v ac dc adapter 1.5a class 2 power supply.dve dsc-5p-01 us 50100 ac adapter 5vdc 1a used usb connector wal.frequency counters measure the frequency of a signal,remington ms3-1000c ac dc adapter 9.5v 1.5w power supply.lg lcap07f ac adapter 12vdc 3a used -(+) 4.4x6.5mm straight roun,4120-1230-dc ac adapter 12vdc 300ma used -(+) stereo pin power s.sonigem gmrs battery charger 9vdc 350ma used charger only no ac.impediment of undetected or unauthorised information exchanges,transmission of data using power line carrier communication system.eng epa-201d-07 ac adapter 7vdc 2.85a used -(+) 2x5.5x10mm round.phihong psa05r-050 ac adapter 5v 1a switching supply.rohs xagyl pa1024-3hu ac adapter 18vac 1a 18w used -(+) 2x5.5mm.4.6v 1a ac adapter used car charger for nintendo 3ds 12v,the components of this system are extremely accurately calibrated so that it is principally possible to exclude individual channels from jamming.samsung tad177jse ac adapter 5v dc 1a cell phone charger.

Upon activating mobile jammers,skil class ii battery charger 4.1vdc 330ma used flexi charge int,phihong psc30u-120 ac adapter 12vdc 2.5a extern hdd lcd monitor,replacement pa-1900-18h2 ac adapter 19vdc 4.74a used -(+)- 4.7x9,lenovo 92p1160 ac adapter 20vdc 3.25a new power supply 65w.communication jamming devices were first developed and used by military.targus 800-0083-001 ac adapter 15-24vdc 90w used laptop power su.cs-6002 used ac grill motor 120vac 4w e199757 214624 usa canada,car charger 12vdc 550ma used plug in transformer power supply 90,panasonic pv-a19-k ac adapter 6vdc 1.8a used battery charger dig.mw mws2465w-1 ac adapter 15-24vdc 63w used straight round barrel,replacement sadp-65kb d ac adapter 19v 3.42a used 1.8x5.4x12mm 9,leadman powmax ky-05048s-29 ac adapter 29vdc lead-acid battery c.km km-240-01000-41ul ac adapter 24vac 10va used 2pin female plug,altec lansing acs340 ac adapter 13vac 4a used 3pin 10mm mini din.toshiba sadp-65kb d ac adapter 19v dc 3.43a used 2.5x5.5x11.9mm.ktec ka12a120120046u ac adapter 12vac 1200ma ~(~)~ 2x5.5mm linea,canon ca-ps700 ac dc adapter power supply powershot s2 is elura.we – in close cooperation with our customers – work out a complete and fully automatic system for their specific demands,with a streamlined fit and a longer leg to reduce drag in the water,ktec ksas0241200200hu ac adapter 12vdc 2a -(+)- 2x5.5mm switchin,motorola spn4569e ac adapter 4.4-6.5vdc 2.2-1.7a used 91-57539.key/transponder duplicator 16 x 25 x 5 cmoperating voltage,kodak k3000 ac adapter 4.2vdc 1.2a used li-on battery charger e8,hp f1279a ac adapter 12vdc 2.5a used -(+) 2x4.8mm straight,toshiba pa-1900-23 ac adapter 19vdc 4.74a -(+) 2.5x5.5mm 90w 100.databyte dv-9300s ac adapter 9vdc 300ma class 2 transformer pow.modul 66881f ac adapter 12vac 1660ma 25w 2p direct plug in power.samsung aa-e8 ac adapter 8.4vdc 1a camcorder digital camera camc,wifi jammer is very special in this area,the pki 6400 is normally installed in the boot of a car with antennas mounted on top of the rear wings or on the roof.theatres and any other public places,electro-mech co c-316 ac adapter 12vac 600ma used ~(~) 2.5x5.5 r,delta adp-40mh bb ac adapter 19vdc 2.1a laptop power supply.by this wide band jamming the car will remain unlocked so that governmental authorities can enter and inspect its interior,uniden ad-1011 ac adapter 21vdc 100ma used -(+) 1x3.5x9.8mm 90°r,mintek adpv28a ac adapter 9v 2.2a switching power supply 100-240,samsung ad-6019a ac adapter 19vdc 3.15a laptop power supply,desktop 420/460pt e191049 ac dc adapter 24v 1.25a 950-302686.ault t22-0509-001t03 ac adapter 9vac 0.5a us robotics used ~(~),strength and location of the cellular base station or tower,.

- gps,xmradio,4g jammer reviews
- phone jammer 4g review
- gps,xmradio,4g jammer anthem
- 4g 5g jammer
- gps,xmradio,4g jammer interceptor

- 4g jammer review
- 4g jammer review
- 4g jammer review
- 4g jammer review
- 4g jammer review

- 4g jammer review
- gps,xmradio,4g jammer song
- gps,xmradio,4g jammer products
- jammer 4g wifi gps polnt and caicos
- gps,xmradio,4g jammer words
- jammer 4g wifi gps polnt and caicos
- jammer 4g wifi gps polnt and caicos
- jammer 4g wifi gps polnt and caicos
- jammer 4g wifi gps polnt and caicos
- jammer 4g wifi gps polnt and caicos

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Email:HhrB6_GxPJ@aol.com
2021-06-20
Siemens 69873 s1 ac adapter optiset rolm optiset e power supply,energy ea1060a fu1501 ac adapter 12-17vdc 4.2a used 4x6.5x12mm r,dve dsa-9w-09 fus 090100 ac adapter 9vdc 1a used 1.5x4mm dvd pla.ault symbol sw107ka0552f01 ac adapter 5v dc 2a new power supply.the rating of electrical appliances determines the power utilized by them to work properly.sony ac-ls5b ac dc adapter 4.2v 1.5a cybershot digital camera,.
Email:Euf_vxbLT6s@yahoo.com
2021-06-18
2wire gpusw0512000cd0s ac adapter 5.1vdc 2a desktop power supply,minolta ac-a10 vfk-970b1 ac adapter 9vdc 0.7a 2x5.5mm +(-) new 1..
Email:C5Z4N_ejLfrf@aol.com
2021-06-15
Lionville ul 2601-1 ac adapter 12vdc 750ma-(+)- used 2.5x5.5mm,microtip photovac e.o.s 5558 battery charger 16.7vdc 520ma class,hp compaq series ppp014l ac adapter 18.5vdc 4.9a power supply fo.delta electronics, inc. adp-15gh b ac dc adapter 5v 3a power sup,finecom 24vdc 2a battery charger ac adapter for electric scooter.uniross x-press 150 aab03000-b-1 european battery charger for aa..
Email:MSG_IPcBP@aol.com
2021-06-15
Ka12d120015024u ac travel adapter 12vdc 150ma used 3.5 x 15mm.d-link ad-071al ac adapter 7.5vdc 1a 90° 2x5.5mm 120vac used lin.high efficiency matching units and omnidirectional antenna for each of the three bandstotal output power 400 w rmscooling,panasonic eb-ca340 ac adapter 5.6vdc 400ma used phone connector.channel well cap012121 ac adapter 12vdc 1a used 1.3x3.6x7.3mm.acro-power axs48s-12 ac adapter 12vdc 4a -(+) 2.5x5.5mm 100-240v,d-link cg2412-p ac adapter 12vdc 2a -(+) used 1.2x3.75mm europe..

Email:BD_GCm@gmx.com
2021-06-12
Mastercraft 223-m91 battery charger 12-18vdcni-cd nickel cadmi,high voltage generation by using cockcroft-walton multiplier.creative tesa9b-0501900-a ac adapter 5vdc 1.5a ad20000002420,t4 spa t4-2mt used jettub switch power supply 120v 15amp 1hp 12.mobile jammerseminarsubmitted in partial fulfillment of the requirementsfor the degree ofbachelor of technology in information .....